File \#: Or2017-567, Version: 1

# CITY COUNCIL <br> COMMITTEE ON ZONING, LANDMARKS AND BUILDING STANDARDS <br> COUNCIL ORDER 

RE: Approval of sign over 100 square feet in area or over 24 feet above grade
ORDERED, that the City Council hereby approves the following sign application submitted by:
Applicant*: pOtf* $t^{\wedge} C U U \sim$ PffcA,^ U(TDVI
(* The Applicant is the owner of the real property or the business tenant of the real property. Do not list the sign contractor, sign erector, sign company or advertising entity in the above space.)

This Order approves the following sign in accordance with Municipal Code of Chicago Section 13-20-680:

Address of Sign: ~7(f?OI
15. CICf YO
(oVf^^^d-
Chicago, IL 606

Zoning District:

DOB Sign Permit Application \#:

Sign Details: ly

1. On-premise /* OR Off-premise
2. Static sign $O R$ Dynamic-image display sign
3. Number of sign faces $\wedge$
4. Projecting over the public way hJ (Yes or No) If yes. Public Way Use \#:
5. Dimensions: Length? $)^{\wedge}$ ) feet Lo inches Height feet inches

Total square feet in area^/^. feet inches SJIQ CkjJrOJiJKSiCi
6. Height above grade: $\sim$ " 7 feet inches
7. Elevation (side of building or lot where the sign will be erected): $\mathrm{CDmCr} \quad{ }^{\prime} \mathrm{J}^{\prime \prime K}{ }^{\circ} 4 \mathrm{CI} \mathrm{CC}$ TO
8. Name of Sign Contractor/Erector: Aril (K.rjhf \&LPjY Inc

To be legal, such sign shall comply with all provisions of Title 17 of the Chicago Municipal Code ("Zoning Ordinance") and all other provisions of the Municipal Code governing the permitting, construction and maintenance and removal of signs and sign structures. Failure of the applicant and the applicant's sijeeassors to comply shall be grounds for invalidation or revocation of the sign permit.

## /Zth

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Alderman Ward
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qaaq

152 f
£|! $=2-6$
$\|^{3}$
$52{ }^{\mathrm{E}}$

- 0 E
not

K

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## LT <br> 13"

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~
```

12'-6"
EXISTING SLAB
$9^{\prime}$-D"
9'-D"
" ${ }^{3} 3^{\prime}-0 " 1$
"3'-0' CONCRETE

| Qn. CONCRETE: 2.3 CU. TOS. | PLAN VIEW |
| :--- | :--- |
| QTY. CONCRETE: 2.0 CU. YDS. EACH | PLAN VIEW |

ELEVATION VIEW

## FOUNDATION NOTE'S:

1. Concrete shall have a minimum compressive strength of $3,000 \mathrm{PSI}$ at 28 days.
2. Caisson footing designed using a soil bearing force of 250 PSF per foot Lateral

DESIGN WIND LOAD: 30.0 PSF
Based on the Chicago Building Code 16 (13-52-310) (f) 1a for solid signs.
SITE:
Ford Cify Mall
7601 South Cicero Avenue
Chicago, Illinois 60652
A 08 Uay 17 RELEASED FOR PERMITTING J.

KV
txsatrnoN

## Robert-James \& Associates, Inc.

12255 West 187th Street. Mokena Illinois 60448-9737 piione: 708-479-83B5 (ax: 708-479-8395 emoil: rin379comcasl.net [http://rin379comcasl.net](http://rin379comcasl.net)
FOUR 31'-6" OAH DIRECT BURY POLES FOR REPLACEMENT ID \& TENANT SIGNS
dRawing number
sheet
1 OF 1
5-05-17
ROBERT-JAMES \& ASSOCIATES, Inc.
Sht 1 of 5
12255 West 187th Street Mokena, Illinois
60448 (708)479-8385

File: QuantumSgn\&FabQ12a.mcd

Site: Ford City Mall
7601 South Cicero Avenue Chicago, Illinois 60652

Project: Design of direct bury pole structures and caisson footings for replacement signage and base trim. Caisson footings will be set placed in cored holes thru existing $l^{\prime}-2 "$ thick slab footing where top of slab is $3-0$ " below grade. This will be done for both the South and North elevation sign pylons. Drawing No. 1705040 rev. A

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Design Wind Load : (PSF) WL :=30.0 Based on the Chicago BuildingCode 16 (13-52-310)(f) la.

Reference: Manual of Steel Construction, AISC 13th Edition.
Tube: ASTMA-500 Gr. B Fy=46.0ksi.; $\quad \mathrm{Fb}=30.36$ ksi.; $\quad \mathrm{Fv}=18.40 \mathrm{ksi}$.

Reference: American Concrete Institute, Code 318.10 Rebar. ASTMA-615
Qade60 Fy $=60.0$ ksi. Concrete : 3,000 psi. compressive strength at 28 days.

Design Loads at Top of Footing, for the $16^{\prime}-0$ " x $25^{\prime}-0$ " Sign Section : ( $3^{*}-0$ " Below Grade.)
Signage:
$+10.0$
SgnTrm := (17.0-25.67-WL>
Base $=38793.3 \mathrm{ft} . \mathrm{Ibs}$.

+ 3.0
(Including 1-0" of base trim and 8 " of side trim.)
'7.0
Base: Base := (7.0-28.42-WL)-

Moment: (ft.Ibs.) MtTOF := SgnTrm + Base MtTOF = 280989.75
Shear: (lbs.) ShrTOF $:=\left(17.0-25.67^{\prime} \mathrm{WL}\right)+(7.0-28.42-\mathrm{WL}) \quad$ ShrTOF $=19059.9$
v|x")","'"//

081-005102 Y ~ LICENSED ' STRUSTUR ENONEFJ

EXPIRES: 11-30-18
MtPoIeTOF $=93663.25$

Design of Pole Structures at Top of Footing for the $16^{\prime}-0^{\prime \prime} \times 25^{\prime}-0{ }^{\prime \prime}$ Sign Section Section Modulus of Tube : (in.*) HSS 10 " x 10 " x $3 / 8^{\prime \prime}$
wall - TubeSM := 40.4
MtTOF
Moment per Pole: (ft.Ibs.) MtPoIeTOF :=
o j o / ■x c MtPoIeTOF-12 ,
Bending Stress : (psi. ) fi, $:=\quad$ fi, $=27820.767$
TubeSM
ShrPoleTOF = 6353.3

Area of Tube : (in.2 ) HSS 10" x 10" x 3/8" wall - TubeArea := 13.2
ShrTOF
Shear per Pole: (lbs.) ShrPoleTOF:

Shear Stress : (psi. ) $\quad \mathrm{f}_{\mathrm{v}}:=$

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Unity Check - Poles: UCPoles :

Design of Caisson Footings : Overturning Moment: (ft.Ibs.) Shear: (lbs.)
Applied Lateral Force ■ (lbs.)
Allowable Lateral Soil Pressure: (lbs.'ft. ${ }^{2}$ per ft.)
Diameter of Round Footing: (ft.)

Distance in Feet From Ground Surface to Point of Application of "P"
Depth of Footing Below the Top of the Existing Slab : (ft.) ( $3^{\prime}-0$ " below grade.)
$\mathrm{Ma}=93663.25 \mathrm{Va}=6353.3 \mathrm{P}=6353.3 \mathrm{LP}:=250$
bl := 3.0
$h=14.742$
$\mathrm{dl}:=8.5$

Allowable Lateral Soil Bearing Pressure Pursuant to the 2012 International Building Code Section 1807.3 . 2.2 and Table 1806.2.
$\mathrm{d} 2=7.902<\mathrm{dl}=8.5$

Check Tensile Stress in Footing:
Overturning Moment About Heel Point: (ft.Ibs.) Mh := Ma+(Va-dl) Treat as a cantilever at bottom.
c Ji-(bll2)
Sw := -:
32
$4>\mathrm{Ft}:=0.65-(5-\mathrm{Vfc})(\mathrm{Mh}-12)^{\prime \prime}$
Compressive Strength of Concrete: (psi.) Yield Strength of Rebar: (psi.)

Section Modulus of Footing: (in. ${ }^{3}$ )

Allowable Concrete Stress: (psi.)
Sw

Tensile Stress in Concrete: (psi.)
(bl 121-10.0

Design of Reinforcing Steel in Caisson : Moment for USD Design : $\quad \mathrm{Mu}:=17-\mathrm{Mh}$
coeff := •
coeff $=0.112$

$$
\mathrm{d}:=[(\mathrm{bll2})-80) \mathrm{Mul} 2
$$

To Plot for "ju ":

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```
    Mh = 147666.3
    fc := 3000 fy := 60000
    Sw}=4580.44
    o>Ft= 178.01
ft = 386.861 > dtFt = 178.01 REBAR REQUIRED FOR STRESS
```

    \(\mathrm{Mu}=251032.71 \mathrm{~d}=15.8\)
    ju := 0.88
    fc-bl-12-d
    ROBERT-JAMES \& ASSOCIATES, Inc.

```
Required Area : (in. }\mp@subsup{}{}{2}\mathrm{ ) Reinforcement Requirment:
    Use yield strength of direct bury tube to check. Yield Strength of Tube (psi.)
            Mu-12
    As:=
            jufyd-0.90
            As}=5.233<\mathrm{ TubeArea = 13.2 No rebar required with the direct bury tube.
```

fy $:=46000 \mathrm{As}=5.233$
\{
$T t-b l d l \wedge 4-27 j$
$0.83-(\mathrm{dl}-0.25) 27$

Note : Keep bottom of tube 3" from bottom of footing to create concrete cover for water exclusion.

## Design Loads at Top of Footing for the 23'-6" x 9'-1 0" Section: ( $3^{\prime}-0$ " Below Grade.)

 2```
Base = 15588.3 ft.Ibs
```

```
Signage: SgnTrm := (24.5-9.83 WL)
7.0,
    +3.0
2
(Including l'-0" of base trim. )
```

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Base: Base := (7.0-11.42-WL)
Moment: ( ft lbs. ) MtTOF := SgnTrm + Base MtTOF $=176345.663$
Shear: (lbs.) ShrTOF := (24.5-9.83-WL) + (7.011.42 WL) $\quad$ ShrTOF $=9623.25$

Design of Pole Structures at Top of Footing for the 23'-6" x 9'-1 0" Section :
Section Modulus of Tube: (in. ${ }^{3}$ ) HSS 14 " x $14^{\prime \prime} \times 3 / 8$ " wall - TubeSM $:=82.5$
d j- $/$ • MtTOF-12
Bending Stress : (psi. ) ft, $:=\quad$ fi, $=25650.278$
TubeSM

Area of Tube : (in. ${ }^{2}$ ) HSS 14"x14"x 3/8" wall - TubeArea := 18.7
ct, ^ / ■-v , ShrTOF
Shear Stress : ( psi. ) $\quad \mathrm{f}_{\mathrm{v}}:=\quad \underset{\text { TubeArea }}{ } \mathrm{f}_{\mathrm{y}}=514.612$
fk f
Unity Check - Poles: UCPoles : $=\quad+--$ UCPoles $=0873<100$ OK

Design of Caisson Footing :

Overturning Moment: ( ft.Ibs. )
Shear: (lbs.)
Applied Lateral Force: ( lbs.)
Allowable Lateral Soil Pressure : (lbs./ft. ${ }^{2}$ per ft.)

| $\mathrm{Ma}:=\mathrm{MtTOF}$ | $\mathrm{Ma}=176345.663$ |
| :--- | :--- |
| $\mathrm{Va}:=$ ShrTOF | $\mathrm{Va}=9623.25$ |
| $\mathrm{P}:=\mathrm{Va}$ | $\mathrm{P}=9623.25$ |
|  | $\mathrm{LP}:=250$ |

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Diameter of Round Footing: ( ft.)
h:-
Distance in Feet From Ground Surface to Point of Application of "P"
Depth of Footing Below the Top of the Existing Slab: (ft.) ( $3^{\prime}-0^{\prime \prime}$ below grade.)
Ph S3bl
d2:=4.25-

Allowable Lateral Soil Bearing Pressure Pursuant to the 2012 International Building Code Section 1807.3.2.2 and Table 1806.2.

Required Depth : (ft.)

$$
\mathrm{bl}:=3.0 \mathrm{~h}=18.325
$$

$$
\mathrm{dl}:=10.5 \mathrm{~S} 3=2625
$$

$\mathrm{d} 2=9.756<\mathrm{d} \mathrm{l}=10.5$

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## Check Tensile Stress in Footing:

Overturning Moment About Heel Point: (ft.Ibs.) Mh := Ma + (Vadl) Treat as a cantilever at bottom.
Compressive Strength of Concrete: ( psi. )
71(bl12)" 32
$\mathrm{rJ}) \mathrm{Ft}:=0.65-(5-\mathrm{v} / \mathrm{fc})$
(Mh-12)" Sw
Yield Strength of Rebar: (psi.)

Section Modulus of Footing: (in. ${ }^{3}$ ) Sw :=

Allowable Concrete Stress : (psi.)

Tensile Stress in Concrete: (psi.) ft :
(bl-12) - 14.0

Design of Reinforcing Steel in Caisson .

Moment for USD Design : $\mathrm{Mu}:=1.7-\mathrm{Mh}$
coeff :=
coeff $=0.165$

$$
\mathrm{d}:=[(\mathrm{bl} 12)-.80] \mathrm{Mu} 2
$$

To Plot for "ju":
$\mathrm{Mh}=277389.787$
fc :=3000 fy := 60000
$\mathrm{Sw}=4580.442$
$\mathrm{d} » \mathrm{Ft}=178.01$
$\mathrm{ft}=726.715>4 * \mathrm{Ft}=178.01$ REBAR REQUIRED FOR STRESS

$$
\mathrm{Mu}=471562.639 \mathrm{~d}=17.8
$$

ju:=0.65
fc-bl-12-d
Use yield strength of direct bury tube to check.

Yield Strength of Tube ■ (psi.) Required Area : (in. ${ }^{2}$ )

Reinforcement Requirment

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Mu-12
jufy-d-0.90

As $=11.814<$ TubeArea $=18.7$ No rebar required with the direct bury tube.
fy $:=46000 \mathrm{As}=11.814$

## ROBERT-JAMES \& ASSOCIATES, Inc.

$\mathrm{CY}=2.229$
Quantity of Concrete . (yds. ${ }^{3}$ ) CY:= 27
V 4-27

Note . Keep bottom of tube 3" from bottom of footing to create concrete cover for water exclusion. «4'-10" EXISTING SLAB

1T-2" " C TO C "

6-3" C TO C

6'3" _"C TO C
.2-6" EXISTING SLAB
$9^{\prime}-0 "$ EXISTING SLAB
$» 3{ }^{\prime}-0 "$
CONCRETE
$\# 3-0 " J$
CONCRETE

QTY. CONCRETE: 2.3 CU. YDS.

QTY. CONCRETE: 2.0 CU. YDS. EACH PLAN VIEW
$-42^{\prime}-5 \%^{\prime \prime}$ BASE --35'-6" SIGNS -

11
-9'-10"--6"-0"-

FQRD
CIT Y
MAI _L
${ }^{6}$-3
стос"

HSS 14" x 14" $\mathrm{t} \mathrm{y}_{2}$ " ASTM A-500 Gr B - EMBEDDED IN FOUNDATION TO WITHIN 3 " OF BOTTOM TO CREATE CONCRETE COVER UNDER POLE.
ELEVATION VIEW
GRADE
S0>.

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THREE (3) HSS $10^{\prime \prime}<10^{\prime \prime}<\mathrm{Vg}^{\prime \prime}$ ASTM A-500 Gr. i -EMBEDDED IN FOUNDATION TO WITHIN $3^{\prime \prime}$ OF BOTTOM TO CREATE CONCRETE COVER UNDER POLE.

SITE:
Ford City Mall
7601 South Cicero Avenue
Chicago, Illinois 60652

FOUNDATION NOTES:

1. Concrete shall hove a minimum compressive strength of $3,000 \mathrm{PSI}$ at 28 days.
2. Caisson footing designed using a soil bearing force of 250 PSF per foot Lateral

DESIGN WIND LOAD: 30.0 PSF
Based on the Chicago Building Code 16 (13-52-310) (f) ta for solid signs.
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$\underset{\text { D }}{\text { APPROVE }}$
Robert-James \& Associates, Inc.
12255 West 187th Street, Mokena Illinois 60448-9737 phone: 708-479-8385 fox: 708-479-8395 email: rjo37§comcast.nel D"1 08 U<7 17
SOU NONE
SHEET
1 OF 1
REV.
A
FOUR 31'-6" OAH DIRECT BURY POLES FOR REPLACEMENT ID \& TENANT SIGNS
I May 17
DRAWING NUMBER
1705040

